

GUIDANCE RELATING TO THE RULES FOR THE CLASSIFICATION OF STEEL SHIPS

(Guidance Part 2 Materials and Welding)

-External Opinion Inquiry-

2019.10.



Machinery Rule Development Team

- Main Amendments -

(1) Enter into force on 1 January 2020 (the date of application for certification of material & welding or the contract date for ship construction)

● To reflect Request for Establishment/Revision of Classification Technical Rules

| Present | Amendment | reason |
|---------|-----------|--------|
|---------|-----------|--------|

Annex 2-1 ~ Annex 2-10 <Omitted>
Annex 2-11 High manganese austenitic steel <New>

Annex 2-1 ~ Annex 2-10 <Omitted>

Annex 2-11 High manganese austenitic steel

1. Application

- (1) This Guidance applies to the high manganese austenitic steel plate(hereinafter referred to as “high manganese austenitic steel”) for cargo tank in ships carrying liquefied natural gases in bulk or for fuel tank in ships using liquefied natural gases as fuels.
- (2) The high manganese austenitic steel used for purposes other than (1) may be applied this Guidance with the approval of the Society.
- (3) The requirements other than those specified in this Guidance are comply with the requirements specified in **Pt 2, Ch 1, 301.** of the Rules.

2. Definitions

- (1) High manganese austenitic steel is the steel with a high amount of manganese in order to retain austenite as its primary phase at atmospheric and service temperature.
- (2) Controlled cooling is a method of cooling from high temperature in accordance with designed cooling rate.

3. Manufacturing process

- (1) Where the high manganese austenitic steel plates are manufactured from the continuous casting slabs, the maximum thickness for approval is to be determined, as a rule, with the roll ratio of 6 as standard. However, upon consideration of the manufacturing process, the roll ratio may be reduced to 4.
- (2) The grade, thickness, deoxidation practice and chemical composition are to comply with the requirements given in **Table 1.**

Table 1 Grade, Thickness, Deoxidation Practice and Chemical Composition

| Grade | Thickne ss, t(mm) | Deoxi dation Practic e | Chemical Composition (%) | | | | | | | | |
|-----------|-------------------------|---------------------------------|--------------------------|-------------------|-------|-------|-------|------|------|-------|------|
| | | | C | Si ⁽¹⁾ | Mn | P | S | Cu | Cr | N | B |
| HMN4 0 | 6 ≤ t ≤ 30 | Killed | 0.35 | 0.10 | 22.50 | 0.030 | 0.010 | 0.30 | 3.00 | 0.050 | 0.00 |
| | | Fine | ~ | ~ | ~ | max. | max. | ~ | ~ | max. | 5 |
| | | grain treated | 0.55 | 0.50 | 25.50 | | | 0.70 | 4.00 | | max. |

NOTES:

- 4 -
 (1) Silicon(Si) may be less than 0.10 %, provided total aluminum is 0.03 % or higher, or provided acid soluble aluminum is 0.025 % or higher.

* It is reflected
 Request for
 Establishment/Revision
 of Classification
 Technical
 Rules(MRD4800-75-20
 19).
 Interim guideline, Part I,
 3. Definitions

 Interim guidelines, Part II 5
 Table 1

| Present | Amendment | reason |
|---------|--|--|
| | <p>4. Heat treatment</p> <p>(1) <u>The heat treatment for high manganese austenitic steel is to be hot rolled and subsequent controlled cooling as necessary.</u></p> <p>(2) <u>Heat treatment following the final rolling process is not permitted.</u></p> <p>5. Selection of test samples</p> <p>(1) <u>One test sample is to be taken from every similarly heat treated piece as rolled directly from one slab or ingot.</u></p> <p>(2) <u>The requirements specified in Pt 2, Ch 1, 301. 6 (4) of the Rules are to be applied to the selection of the test samples.</u></p> <p>6. Selection of test specimens</p> <p>(1) <u>Tensile test specimens are to comply with the requirements shown in (a) to (c) below:</u></p> <p>(a) <u>Tensile test specimens are to be taken according to the requirements specified in Pt 2, Ch 1, 301. 7 (2) of the Rules.</u></p> <p>(b) <u>Normally flat tensile test specimens are to be prepared in such a manner as to maintain the rolling scale at least at one side.</u></p> <p>(c) <u>When instead a machined round tensile test specimen is used then the axis must be located at a position lying at a distance of t/4 from the surface or as near as possible to this position.</u></p> <p>(2) <u>Impact test specimens are to be taken according to the requirements specified in Pt 2, Ch 1, 301. 7 (3) of the Rules.</u></p> <p>7. Mechanical properties</p> <p><u>The mechanical properties of high manganese austenitic steel plates are classified as specified in Table 2.</u></p> | <p>- Interim guideline, Part II, 4.2</p> <p>- ASTM A1106 4.3</p> |

| Present | Amendment | reason | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--------------------------|--|-----------------------------------|---|---|--------------------|--|--|---|---|---|--------------------|--|--|------------------|------------------|-------|----------|-----------|----|------|----|----|--------------------------|-------------------------|-----------------------------------|---------------|---------------|---------------|---|
| | <p data-bbox="875 193 1821 252">Table 2 Mechanical properties for high manganese austenitic steel plates</p> <table border="1" data-bbox="875 264 1821 491"> <thead> <tr> <th rowspan="3">Grade</th> <th colspan="3">Tensile test</th> <th colspan="2">Impact test</th> </tr> <tr> <th rowspan="2">Yield Strength (<i>N/mm²</i>)</th> <th rowspan="2">Tensile Strength (<i>N/mm²</i>)</th> <th rowspan="2">Elongation ($L = 5.65\sqrt{A}$) (%)</th> <th rowspan="2">Test Temp. (°C)</th> <th colspan="2">Average Impact Energy(J) min.⁽¹⁾</th> </tr> <tr> <th>L⁽²⁾</th> <th>T⁽²⁾</th> </tr> </thead> <tbody> <tr> <td>HMN40</td> <td>min. 400</td> <td>800 ~ 970</td> <td>22</td> <td>-196</td> <td>41</td> <td>27</td> </tr> </tbody> </table> <p data-bbox="875 501 1821 719"> NOTE: (1) When the absorbed energy of two or more test specimens among a set of test specimens is less in value than the specified average absorbed energy or when the absorbed energy of a single test specimen is less in value than 70 % of the specified average absorbed energy, the test is considered to be failed. (2) L (or T) denotes that the longitudinal axis of the test specimen is arranged parallel (or transverse) to the final direction of rolling. </p> <p data-bbox="875 756 1821 783">8. Welding consumables for high manganese austenitic steel</p> <p data-bbox="875 799 1821 858">(1) Where no special requirements are given in 8, those as specified in Pt 2, Ch 2, 607. of the Rules apply in analogous manner.</p> <p data-bbox="875 863 1821 890">(2) Welding consumables are classified as specified in Table 3.</p> <p data-bbox="875 927 1821 954">Table 3 Grades and Marks of Welding Consumables</p> <table border="1" data-bbox="875 967 1731 1098"> <thead> <tr> <th>Material for TIG welding</th> <th>Flux cored wire welding</th> <th>Consumables for submerged welding</th> </tr> </thead> <tbody> <tr> <td><i>RY HMN</i></td> <td><i>RW HMN</i></td> <td><i>RU HMN</i></td> </tr> </tbody> </table> <p data-bbox="875 1139 1821 1230">(3) Submerged arc welding consumables which have passed the tests for each welding process are to be appended with the suffixes shown in Table 4 at the end of their marks.</p> | Grade | Tensile test | | | Impact test | | Yield Strength (<i>N/mm²</i>) | Tensile Strength (<i>N/mm²</i>) | Elongation ($L = 5.65\sqrt{A}$) (%) | Test Temp. (°C) | Average Impact Energy(J) min. ⁽¹⁾ | | L ⁽²⁾ | T ⁽²⁾ | HMN40 | min. 400 | 800 ~ 970 | 22 | -196 | 41 | 27 | Material for TIG welding | Flux cored wire welding | Consumables for submerged welding | <i>RY HMN</i> | <i>RW HMN</i> | <i>RU HMN</i> | <p data-bbox="1839 220 2148 323">Interim guidelines, Part II, 6 Mechanical properties Table 2</p> |
| Grade | Tensile test | | | Impact test | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Yield Strength (<i>N/mm²</i>) | | Tensile Strength (<i>N/mm²</i>) | Elongation ($L = 5.65\sqrt{A}$) (%) | Test Temp. (°C) | Average Impact Energy(J) min. ⁽¹⁾ | | | | | | | | | | | | | | | | | | | | | | | |
| | | L ⁽²⁾ | | | | T ⁽²⁾ | | | | | | | | | | | | | | | | | | | | | | | |
| HMN40 | min. 400 | 800 ~ 970 | 22 | -196 | 41 | 27 | | | | | | | | | | | | | | | | | | | | | | | |
| Material for TIG welding | Flux cored wire welding | Consumables for submerged welding | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <i>RY HMN</i> | <i>RW HMN</i> | <i>RU HMN</i> | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| Present | Amendment | reason | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---------------------------------|---|---------------------------|--|-----------------------------|-----------------------------|---------------------------|---------------------------|---------------------------------|----------------------------|---------------|--------------------------|--|--|--|--|--|--|--|--|--|----------|-----------|-----------|----------|----------|-----------|-----------|-----------|----------|---------------|---------------|---------------------------|---------------------------|--|----------------------------|-----------------------------|---------------------------|---------------------------|---------------------------|---------------------------|----------|-------|--------------------------|--|--|--|--|--|--|--|--|--|----------|-----------|-----------|----------|----------|-----------|-----------|-----------|----------|---------------|---------------|---------------------------|---------------------------|--|-----------------------------|-----------------------------|---------------------------|---------------------------|---------------------------|----------------------------|----------|--|
| | <p>Table 4 Marks</p> <table border="1" data-bbox="887 225 1823 411"> <thead> <tr> <th>Welding technique</th> <th>Marks</th> </tr> </thead> <tbody> <tr> <td>Multi-run technique</td> <td><u>M</u></td> </tr> <tr> <td>Two-run technique</td> <td><u>T</u></td> </tr> <tr> <td>Multi-run and Two-run technique</td> <td><u>TM</u></td> </tr> </tbody> </table> <p>(4) Deposited metal test (A) Chemical composition (a) Deposited metals of welding consumables for flux cored wire welding and submerged arc welding are to have the chemical composition given in Table 5 and Table 6 respectively. (b) TIG welding consumables are to have the chemical composition of ladle analysis value complied with the requirements as given in Table 7.</p> <p>Table 5 Chemical Composition of Deposited Metal for Flux Cored Wire Welding</p> <table border="1" data-bbox="862 871 1823 1118"> <thead> <tr> <th rowspan="2">Grade</th> <th colspan="10">Chemical composition (%)</th> </tr> <tr> <th><u>C</u></th> <th><u>Si</u></th> <th><u>Mn</u></th> <th><u>P</u></th> <th><u>S</u></th> <th><u>Ni</u></th> <th><u>Cr</u></th> <th><u>Mo</u></th> <th><u>N</u></th> <th><u>Others</u></th> </tr> </thead> <tbody> <tr> <td><u>RW HMN</u></td> <td><u>0.2~</u> <u>0.5</u></td> <td><u>0.2~</u> <u>1.0</u></td> <td><u>18.0</u> <u>~26.</u> <u>0</u></td> <td><u>0.02</u> <u>max.</u></td> <td><u>0.015</u> <u>max.</u></td> <td><u>5.0</u> <u>max.</u></td> <td><u>5.0</u> <u>max.</u></td> <td><u>2.5</u> <u>max.</u></td> <td><u>0.1</u> <u>max.</u></td> <td><u>—</u></td> </tr> </tbody> </table> <p>Table 6 Chemical Composition of Deposited Metal for Submerged Arc Welding</p> <table border="1" data-bbox="862 1198 1823 1445"> <thead> <tr> <th rowspan="2">Grade</th> <th colspan="10">Chemical composition (%)</th> </tr> <tr> <th><u>C</u></th> <th><u>Si</u></th> <th><u>Mn</u></th> <th><u>P</u></th> <th><u>S</u></th> <th><u>Ni</u></th> <th><u>Cr</u></th> <th><u>Mo</u></th> <th><u>N</u></th> <th><u>Others</u></th> </tr> </thead> <tbody> <tr> <td><u>RU HMN</u></td> <td><u>0.2~</u> <u>0.6</u></td> <td><u>1.5</u> <u>max.</u></td> <td><u>18.0</u> <u>~26.</u> <u>0</u></td> <td><u>0.020</u> <u>max.</u></td> <td><u>0.015</u> <u>max.</u></td> <td><u>3.0</u> <u>max.</u></td> <td><u>5.0</u> <u>max.</u></td> <td><u>2.5</u> <u>max.</u></td> <td><u>0.10</u> <u>max.</u></td> <td><u>—</u></td> </tr> </tbody> </table> | Welding technique | Marks | Multi-run technique | <u>M</u> | Two-run technique | <u>T</u> | Multi-run and Two-run technique | <u>TM</u> | Grade | Chemical composition (%) | | | | | | | | | | <u>C</u> | <u>Si</u> | <u>Mn</u> | <u>P</u> | <u>S</u> | <u>Ni</u> | <u>Cr</u> | <u>Mo</u> | <u>N</u> | <u>Others</u> | <u>RW HMN</u> | <u>0.2~</u> <u>0.5</u> | <u>0.2~</u> <u>1.0</u> | <u>18.0</u> <u>~26.</u> <u>0</u> | <u>0.02</u> <u>max.</u> | <u>0.015</u> <u>max.</u> | <u>5.0</u> <u>max.</u> | <u>5.0</u> <u>max.</u> | <u>2.5</u> <u>max.</u> | <u>0.1</u> <u>max.</u> | <u>—</u> | Grade | Chemical composition (%) | | | | | | | | | | <u>C</u> | <u>Si</u> | <u>Mn</u> | <u>P</u> | <u>S</u> | <u>Ni</u> | <u>Cr</u> | <u>Mo</u> | <u>N</u> | <u>Others</u> | <u>RU HMN</u> | <u>0.2~</u> <u>0.6</u> | <u>1.5</u> <u>max.</u> | <u>18.0</u> <u>~26.</u> <u>0</u> | <u>0.020</u> <u>max.</u> | <u>0.015</u> <u>max.</u> | <u>3.0</u> <u>max.</u> | <u>5.0</u> <u>max.</u> | <u>2.5</u> <u>max.</u> | <u>0.10</u> <u>max.</u> | <u>—</u> | |
| Welding technique | Marks | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Multi-run technique | <u>M</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Two-run technique | <u>T</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Multi-run and Two-run technique | <u>TM</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Grade | Chemical composition (%) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | <u>C</u> | <u>Si</u> | <u>Mn</u> | <u>P</u> | <u>S</u> | <u>Ni</u> | <u>Cr</u> | <u>Mo</u> | <u>N</u> | <u>Others</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | <u>C</u> | <u>Si</u> | <u>Mn</u> | <u>P</u> | <u>S</u> | <u>Ni</u> | <u>Cr</u> | <u>Mo</u> | <u>N</u> | <u>Others</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <u>RU HMN</u> | <u>0.2~</u> <u>0.6</u> | <u>1.5</u> <u>max.</u> | <u>18.0</u> <u>~26.</u> <u>0</u> | <u>0.020</u> <u>max.</u> | <u>0.015</u> <u>max.</u> | <u>3.0</u> <u>max.</u> | <u>5.0</u> <u>max.</u> | <u>2.5</u> <u>max.</u> | <u>0.10</u> <u>max.</u> | <u>—</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| Present | Amendment | reason | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--|----------------------------|-----------------------------|-----------------------------|----------|-----------|-----------|-----------|----------|--------|--|--|----------|-----------|-----------|----------|----------|-----------|-----------|-----------|----------|--------|-----------|------|------|------|-------|-------|-----|-----|-----|------|---|------------|-----|-----|-----------|------|------|------|------|------|------|---|--------------|--|--|----------------------------|--|--|--|-------------------|--------------------|-----------------------------|----------|----------|---------|------|---------|--|-----------|----------------------------|--|--------------------|-----------------------------|----------|--|------|---------|---|
| | <p data-bbox="864 185 1709 209">Table 7 Chemical Composition of Deposited Metal for TIG Electrodes</p> <table border="1" data-bbox="864 225 1834 443"> <thead> <tr> <th data-bbox="864 225 965 272" rowspan="2">Grade</th> <th colspan="10" data-bbox="965 225 1834 272">Chemical composition (%)</th> </tr> <tr> <th data-bbox="965 272 1055 316"><i>C</i></th> <th data-bbox="1055 272 1144 316"><i>Si</i></th> <th data-bbox="1144 272 1234 316"><i>Mn</i></th> <th data-bbox="1234 272 1323 316"><i>P</i></th> <th data-bbox="1323 272 1413 316"><i>S</i></th> <th data-bbox="1413 272 1503 316"><i>Ni</i></th> <th data-bbox="1503 272 1592 316"><i>Cr</i></th> <th data-bbox="1592 272 1682 316"><i>Mo</i></th> <th data-bbox="1682 272 1771 316"><i>N</i></th> <th data-bbox="1771 272 1834 316">Others</th> </tr> </thead> <tbody> <tr> <td data-bbox="864 320 965 368"><i>RY</i></td> <td data-bbox="965 320 1055 368">0.2~</td> <td data-bbox="1055 320 1144 368">0.1~</td> <td data-bbox="1144 320 1234 368">18.0</td> <td data-bbox="1234 320 1323 368">0.020</td> <td data-bbox="1323 320 1413 368">0.015</td> <td data-bbox="1413 320 1503 368">5.0</td> <td data-bbox="1503 320 1592 368">5.0</td> <td data-bbox="1592 320 1682 368">2.5</td> <td data-bbox="1682 320 1771 368">0.10</td> <td data-bbox="1771 320 1834 368">—</td> </tr> <tr> <td data-bbox="864 368 965 443"><i>HMN</i></td> <td data-bbox="965 368 1055 443">0.5</td> <td data-bbox="1055 368 1144 443">1.0</td> <td data-bbox="1144 368 1234 443">~26. 0</td> <td data-bbox="1234 368 1323 443">max.</td> <td data-bbox="1323 368 1413 443">max.</td> <td data-bbox="1413 368 1503 443">max.</td> <td data-bbox="1503 368 1592 443">max.</td> <td data-bbox="1592 368 1682 443">max.</td> <td data-bbox="1682 368 1771 443">max.</td> <td data-bbox="1771 368 1834 443">—</td> </tr> </tbody> </table> <p data-bbox="927 483 1834 539">(B) Mechanical properties for deposited metal are to comply with the requirements in Table 8.</p> <p data-bbox="846 584 1464 608">Table 8 Mechanical properties for Deposited Metal</p> <table border="1" data-bbox="846 616 1778 818"> <thead> <tr> <th colspan="3" data-bbox="846 616 1368 659">Tensile test</th> <th colspan="2" data-bbox="1368 616 1778 659">Charpy V notch Impact test</th> </tr> <tr> <th data-bbox="846 659 1028 767">Yield strength (N/mm²)</th> <th data-bbox="1028 659 1209 767">Tensile strength (N/mm²)</th> <th data-bbox="1209 659 1368 767">Elongation (%)</th> <th data-bbox="1368 659 1550 767">Test temp. (°C)</th> <th data-bbox="1550 659 1778 767">Average absorbed energy (J)</th> </tr> </thead> <tbody> <tr> <td data-bbox="846 767 1028 818">400 min.</td> <td data-bbox="1028 767 1209 818">660 min.</td> <td data-bbox="1209 767 1368 818">22 min.</td> <td data-bbox="1368 767 1550 818">-196</td> <td data-bbox="1550 767 1778 818">27 min.</td> </tr> </tbody> </table> <p data-bbox="887 882 1834 970">(5) Butt weld test Mechanical properties for butt weld test are to comply with the requirements in Table 9.</p> <p data-bbox="909 1031 1503 1054">Table 9 Mechanical properties for butt weld test</p> <table border="1" data-bbox="909 1062 1834 1326"> <thead> <tr> <th data-bbox="909 1062 1016 1193" rowspan="2">Yield strength (N/mm²)</th> <th data-bbox="1016 1062 1447 1193" rowspan="2">Bend test</th> <th colspan="2" data-bbox="1447 1062 1834 1106">Charpy V notch Impact test</th> </tr> <tr> <th data-bbox="1447 1106 1581 1193">Test temp. (°C)</th> <th data-bbox="1581 1106 1834 1193">Average absorbed energy (J)</th> </tr> </thead> <tbody> <tr> <td data-bbox="909 1193 1016 1326">660 min.</td> <td data-bbox="1016 1193 1447 1326">The test specimens are to be capable of withstanding, without crack exceeding 3 mm long on the outer surface of the specimen or other defects.</td> <td data-bbox="1447 1193 1581 1326">-196</td> <td data-bbox="1581 1193 1834 1326">27 min.</td> </tr> </tbody> </table> | Grade | Chemical composition (%) | | | | | | | | | | <i>C</i> | <i>Si</i> | <i>Mn</i> | <i>P</i> | <i>S</i> | <i>Ni</i> | <i>Cr</i> | <i>Mo</i> | <i>N</i> | Others | <i>RY</i> | 0.2~ | 0.1~ | 18.0 | 0.020 | 0.015 | 5.0 | 5.0 | 2.5 | 0.10 | — | <i>HMN</i> | 0.5 | 1.0 | ~26. 0 | max. | max. | max. | max. | max. | max. | — | Tensile test | | | Charpy V notch Impact test | | Yield strength (N/mm ²) | Tensile strength (N/mm ²) | Elongation (%) | Test temp. (°C) | Average absorbed energy (J) | 400 min. | 660 min. | 22 min. | -196 | 27 min. | Yield strength (N/mm ²) | Bend test | Charpy V notch Impact test | | Test temp. (°C) | Average absorbed energy (J) | 660 min. | The test specimens are to be capable of withstanding, without crack exceeding 3 mm long on the outer surface of the specimen or other defects. | -196 | 27 min. | <p data-bbox="1839 655 2085 767">- IMO MSC. 1/Circ.1599 Annex 6.2 Table 3</p> |
| Grade | Chemical composition (%) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | <i>C</i> | <i>Si</i> | <i>Mn</i> | <i>P</i> | <i>S</i> | <i>Ni</i> | <i>Cr</i> | <i>Mo</i> | <i>N</i> | Others | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <i>RY</i> | 0.2~ | 0.1~ | 18.0 | 0.020 | 0.015 | 5.0 | 5.0 | 2.5 | 0.10 | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <i>HMN</i> | 0.5 | 1.0 | ~26. 0 | max. | max. | max. | max. | max. | max. | — | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Tensile test | | | Charpy V notch Impact test | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Yield strength (N/mm ²) | Tensile strength (N/mm ²) | Elongation (%) | Test temp. (°C) | Average absorbed energy (J) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 400 min. | 660 min. | 22 min. | -196 | 27 min. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Yield strength (N/mm ²) | Bend test | Charpy V notch Impact test | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | Test temp. (°C) | Average absorbed energy (J) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 660 min. | The test specimens are to be capable of withstanding, without crack exceeding 3 mm long on the outer surface of the specimen or other defects. | -196 | 27 min. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| Present | Amendment | reason |
|---------|--|---|
| | <p>(6) Fillet weld test <u>Fillet weld test is to be in accordance with the requirements in Pt 2, Ch 2, 602. 7 of the Rules.</u></p> <p>9. Welder</p> <p>(1) <u>Welders for high manganese austenitic steel are to have a qualification by welder qualification test with high manganese austenitic steel specimen in accordance with Pt 2, Ch 2, Sec. 5 of the Rules.</u></p> <p>(2) <u>Welders who engage in welding for high manganese austenitic steel is to have passed qualification test with high manganese austenitic steel.</u></p> <p>10. Welding procedure qualification tests</p> <p>(1) <u>Welding procedure qualification tests for high manganese austenitic steel is to be in accordance with the requirements in Pt 7, Ch 5, Sec 6 of Rules and Rules/Guidances for the Classification of Ships Using Low-flashpoint Fuels.</u></p> <p>(2) <u>The welding procedure qualification test is carried out considering the following points.</u></p> <p>(A) <u>Special attention is to be given to the first root pass when applying flux-cored arc welding (FCAW); reduced amperage is to be considered. And weld gas composition of FCAW is to be normally an 80/20 mix of argon and carbon dioxide.</u></p> <p>(B) <u>Welding heat input is to be controlled equal to maximum 30 kJ/cm or below.</u></p> <p>11. Welding practice</p> <p>(1) <u>Distance between the weld and nozzle is to be kept to a minimum to reduce the oxygen content at the vicinity of the weld pool.</u></p> <p>(2) <u>Appropriate ventilation is to be provided to reduce exposure to hazardous welding fumes.</u></p> <p>(3) <u>The edges to be welded are to be smooth, uniform and free from moisture, grease, rust and paint which may cause injurious defects in welded joints.</u></p> <p>12. Marking</p> <p>(1) <u>Steel plates which have satisfactorily complied with the required tests are to be marked with the identification mark in accordance with Pt 2, Ch 1, 301. 11 of the Rules.</u></p> <p>(2) <u>Where the plates are controlled cooling : CC (e.g. : HMN40 CC)</u></p> | <p>- IMO MSC. 1/Circ.1599 Annex 10.6.2.1.1 10.6.2.3 10.6.2.1.2</p> <p>- IMO MSC. 1/Circ.1599 Annex 10.6.2.2 10.6.2.4</p> |