# Amended Guidance for the Classification of Ships Using Low-flashpoint Fuels

Dec. 2019

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# - Main Amendments -

**(1) Enter into force on 1 January 2020 (the contract date for ship construction)**

◉ To reflect Request for Establishment/Revision of Classification Technical Rules

| Present | Amendment |
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| **CHAPTER 6 FUEL CONTAINMENT SYSTEM** | **CHAPTER 6 FUEL CONTAINMENT SYSTEM** |
| **Section 3 <Omitted>** | **Section 3 <Sames as the present guidance>** |
| **Section 4 Liquefied gas fuel containment** | **Section 4 Liquefied gas fuel containment** |
| **408. <Omitted>** | **408. <Sames as the present guidance>** |
| **413. Materials and construction** | **413. Materials and construction** |
| **1. ~ 5. <Omitted>** | **1. ~ 5. <Same as the present guidance>** |
| **6. <New>** | **6.** The high manganese austenitic steel for fuel tank for the carriage of liquefied natural gases is to comply with **Annex 2**. *(2020)* |

| Present | Amendment |
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| **Annex 1** **<Omitted>**<br><br>**Annex 2 High manganese austenitic steel for Cryogenic Service <New>** | **Annex 1** **<Omitted>**<br><br>**Annex 2 High manganese austenitic steel for Cryogenic Service**<br><br>**Section 1 General**<br><br>**101. Scope**<br>**1.** This Annex provides the designer and manufacturer with practical information on the design and construction of fuel tanks using high manganese austenitic steel for cryogenic service to comply with the Design Conditions defined in **Rules for Ships using low-flashpoint fuels, Chapter 6, 412**.<br><br>**102. Application**<br>**1.** This Annex are not intended to replace any requirements of **Rules for Ships using low-flashpoint fuels**. They are intended as complementary guidelines on how to utilize high manganese austenitic steel in the design and fabrication of fuel tanks complying with the **Rules for Ships using low-flashpoint fuels**.<br><br>**103. Definitions**<br>**1. Under-matched welds** means for welded connections where the weld metal has lower yield- or tensile-strength than the parent metal.<br><br>**Section 2 Application**<br><br>**201. Design application**<br>**1.** The relevant load conditions and design conditions should be established in accordance with **Rules for Ships using low-flashpoint fuels, Chapter 6, 412**. A guidance on special considerations to the high manganese austenitic steel is described beolw.<br>**2.** For the selection of relevant safety factors for high manganese austenitic steels(see **Rules for Ships using low-flashpoint fuels, Chapter 6, 415**), the safety factors specified for “Austenitic Steels“ should be applied both for base material and for as welded condition |

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| | **202. Ultimate design condition**<br>**1.** It should be noted that high manganese austenitic steels normally have under-matched welds and, therefore, it is of great importance that the design values of the yield strength and tensile strength are based on the “minimum mechanical properties“ for the base material and as welded condition(see 6 Mechanical Properties). Note the limitation to under-matched welds defined in **Rules for Ships using low-flashpoint fuels, Chapter 16, 303.5.(1)**.<br><br>**203. Buckling strength**<br>**1.** Buckling strength analysis should be carried out based on recognized standards. Functional loads as defined in **Rules for Ships using low-flashpoint fuels, Chapter 6, 401.6** should be considered. Note that design tolerances should be considered where relevant and be included in the strength assessment as required in **Rules for Ships using low-flashpoint fuels, Chapter 16, 402**.<br><br>**204. Fatigue design condition**<br>**1.** The fatigue design curves for base material and for butt weld joint should use S-N curve of D grade in IIW.<br>**2.** The fatigue design curves for other weld joints except butt weld joint should be agreed with the Society.<br>**3.** Design S-N curve given in Table 1 correspond to a probability of survival of 97.6%. |

Table 1 S-N curves in air

| S-N curve | $N \leq 10^7$ cycles | | $N > 10^7$ cycles | Fatigue limit at $10^7$ cycle(MPa) | Thickness exponent k |
| --- | --- | --- | --- | --- | --- |
| | $m_1$ | $\log \bar{a}_1$ | $\log \bar{a}_2$, $m_2 = 5.0$ | | |
| D | 3.0 | 12.164 | 15.606 | 52.63 | 0.20 |

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| | **205. Fracture mechanics analyses**<br><br>**1.** For a fuel tank where a reduced secondary barrier is applied, fracture mechanics analysis should be carried out in accordance with **Rules for Ships using low-flashpoint fuels**.<br><br>**2.** Fracture toughness properties should be expressed using recognized standards. Depending on the material, fracture toughness properties determined for loading rates similar to those expected in the tank system should be required. The fatigue crack propagation rate properties should be documented for the tank material and its welded joints for the relevant service conditions. These properties should be expressed using a recognized fracture mechanics practice relating the fatigue crack propagation rate to the variation in stress intensity, $\triangle K$, at the crack tip. The effect of stresses produced by static loads should be taken into account when establishing the choice of fatigue crack propagation rate parameters.<br><br>**3.** Note that for the application where very high static load utilization is relevant, alternative methods such as ductile fracture mechanics analysis should be considered.<br><br>**4.** A fracture mechanics analysis is required for type B tank(**Rules for Ships using low-flashpoint fuels, Chapter 16, 415.2.(3).(C)**) where a reduced secondary barrier is applied. Fracture mechanics analysis may also be required for other tank types as found relevant to show compliance with fatigue and crack propagation properties. Note that CTOD values used in fracture mechanics analysis may in any case be an important property to analyze to ensure that materials are considered suitable for the application. |

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| | **206. Welding**<br><br>**1.** Welding should be carried out in accordance with **Rules for Ships using low-flashpoint fuels, Chapter 16, Section 3**.<br><br>**2.** For welding the following points can be considered:<br>(1) For reducing the heat input during production:<br>(A) special attention should be given to the first root pass when applying flux-cored arc welding(FCAW); reduced amperage should be considered;<br>(B) welding heat input is to be equal to 30 kJ/cm or below;<br>(2) Distance between the weld and nozzle should be kept to a minimum to reduce the oxygen content at the vicinity of the weld pool;<br>(3) Weld gas composition of FCAW should normally be an 80/20 mix of argon and carbon dioxide; and<br>(4) Appropriate ventilation should be provided to reduce exposure to hazardous welding fumes.<br><br>**207. Non-destructive testing(NDT)**<br><br>**1.** The scope of non-destructive testing(NDT) should be as required by **Rules for Ships using low-flashpoint fuels, Chapter 16, 306**. NDT procedures should be in accordance with recognized standards to the satisfaction of the Society. For high manganese austenitic steel suitable NDT procedure normally applicable for austenitic steels should be used.<br><br>**208. Corrosion resistance**<br><br>**1.** High manganese austenitic steel is not considered a very strong corrosion resistant material in line with several similar materials such as 304 stainless steel. Particularly for LNG fuel tanks that may not be in operation, appropriate environment should be maintained to prevent corrosion. |