

# Amended Guidances for the Classification of Steel Ships

## (Part 2 Materials and Welding)

Dec. 2019



KR

Effective date : 1 Jan. 2020

(1) **Date of application for certification of material & welding or the contract date for ship construction**

● To reflect Request for Establishment/Revision of Classification Technical Rules (MSC.1/Circ. 1599)



Present	Amendment																																																							
<p data-bbox="369 172 958 204">Annex 2-1 ~ Annex 2-10 &lt;Omitted&gt;</p> <p data-bbox="421 236 947 300"><u>Annex 2-11 High manganese austenitic steel &lt;New&gt;</u></p>	<p data-bbox="1205 172 1794 204">Annex 2-1 ~ Annex 2-10 &lt;Omitted&gt;</p> <p data-bbox="1070 236 1939 268"><u>Annex 2-11 High manganese austenitic steel (2020)</u></p> <p data-bbox="994 320 1178 347"><b>1. Application</b></p> <p data-bbox="1028 363 1977 480">(1) This Guidance applies to the high manganese austenitic steel plate(herein-after referred to as “high manganese austenitic steel“) for cargo tank in ships carrying liquefied natural gases in bulk or for fuel tank in ships using liquefied natural gases as fuels.</p> <p data-bbox="1028 488 1977 544">(2) The high manganese austenitic steel used for purposes other than (1) may be applied this Guidance with the approval of the Society.</p> <p data-bbox="1028 552 1977 608">(3) The requirements other than those specified in this Guidance are comply with the requirements specified in <b>Pt 2, Ch 1, 301.</b> of the Rules.</p> <p data-bbox="994 624 1171 651"><b>2. Definitions</b></p> <p data-bbox="1028 667 1977 751">(1) High manganese austenitic steel is the steel with a high amount of manganese in order to retain austenite as its primary phase at atmospheric and service temperature.</p> <p data-bbox="1028 759 1977 815">(2) Controlled cooling is a method of cooling from high temperature in accordance with designed cooling rate.</p> <p data-bbox="994 831 1328 858"><b>3. Manufacturing process</b></p> <p data-bbox="1028 874 1977 1023">(1) Where the high manganese austenitic steel plates are manufactured from the continuous casting slabs, the maximum thickness for approval is to be determined, as a rule, with the roll ratio of 6 as standard. However, upon consideration of the manufacturing process, the roll ratio may be reduced to 4.</p> <p data-bbox="1028 1031 1977 1086">(2) The grade, thickness, deoxidation practice and chemical composition are to comply with the requirements given in <b>Table 1.</b></p> <p data-bbox="1032 1118 1951 1145"><b>Table 1 Grade, Thickness, Deoxidation Practice and Chemical Composition</b></p> <table border="1" data-bbox="1032 1158 1977 1453"> <thead> <tr> <th rowspan="2">Grade</th> <th rowspan="2">Thickne ss, t(mm)</th> <th rowspan="2">Deoxi dation Practic e</th> <th colspan="9">Chemical Composition (%)</th> </tr> <tr> <th><i>C</i></th> <th><i>Si</i><sup>(1)</sup></th> <th><i>Mn</i></th> <th><i>P</i></th> <th><i>S</i></th> <th><i>Cu</i></th> <th><i>Cr</i></th> <th><i>N</i></th> <th><i>B</i></th> </tr> </thead> <tbody> <tr> <td rowspan="2">HMN40</td> <td rowspan="2">6 ≤ t ≤ 30</td> <td>Killed and Fine grain treated</td> <td>0.35</td> <td>0.10</td> <td>22.50</td> <td>0.030</td> <td>0.010</td> <td>0.30</td> <td>3.00</td> <td>0.050</td> <td>0.00</td> </tr> <tr> <td></td> <td>~</td> <td>~</td> <td>~</td> <td>max.</td> <td>max.</td> <td>~</td> <td>~</td> <td>max.</td> <td>5 max.</td> </tr> <tr> <td></td> <td></td> <td></td> <td>0.55</td> <td>0.50</td> <td>25.50</td> <td></td> <td></td> <td>0.70</td> <td>4.00</td> <td></td> <td></td> </tr> </tbody> </table> <p data-bbox="1039 1465 1133 1492">NOTES:</p> <p data-bbox="1070 1501 1977 1557">(1) Silicon(Si) may be less than 0.10 %, provided total aluminum is 0.03 % or higher, or provided acid soluble aluminum is 0.025 % or higher.</p>	Grade	Thickne ss, t(mm)	Deoxi dation Practic e	Chemical Composition (%)									<i>C</i>	<i>Si</i> <sup>(1)</sup>	<i>Mn</i>	<i>P</i>	<i>S</i>	<i>Cu</i>	<i>Cr</i>	<i>N</i>	<i>B</i>	HMN40	6 ≤ t ≤ 30	Killed and Fine grain treated	0.35	0.10	22.50	0.030	0.010	0.30	3.00	0.050	0.00		~	~	~	max.	max.	~	~	max.	5 max.				0.55	0.50	25.50			0.70	4.00		
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Present	Amendment
	<p><b>4. Heat treatment</b></p> <p>(1) <u>The heat treatment for high manganese austenitic steel is to be hot rolled and subsequent controlled cooling as necessary.</u></p> <p>(2) <u>Heat treatment following the final rolling process is not permitted.</u></p> <p><b>5. Selection of test samples</b></p> <p>(1) <u>One test sample is to be taken from every similarly heat treated piece as rolled directly from one slab or ingot.</u></p> <p>(2) <u>The requirements specified in <b>Pt 2, Ch 1, 301. 6</b> (4) of the Rules are to be applied to the selection of the test samples.</u></p> <p><b>6. Selection of test specimens</b></p> <p>(1) <u>Tensile test specimens are to comply with the requirements shown in (a) to (c) below:</u></p> <p>(a) <u>Tensile test specimens are to be taken according to the requirements specified in <b>Pt 2, Ch 1, 301. 7</b> (2) of the Rules.</u></p> <p>(b) <u>Normally flat tensile test specimens are to be prepared in such a manner as to maintain the rolling scale at least at one side.</u></p> <p>(c) <u>When instead a machined round tensile test specimen is used then the axis must be located at a position lying at a distance of t/4 from the surface or as near as possible to this position.</u></p> <p>(2) <u>Impact test specimens are to be taken according to the requirements specified in <b>Pt 2, Ch 1, 301. 7</b> (3) of the Rules.</u></p> <p><b>7. Mechanical properties</b></p> <p><u>The mechanical properties of high manganese austenitic steel plates are classified as specified in <b>Table 2</b>.</u></p>

**Present**

**Amendment**

**Table 2 Mechanical properties for high manganese austenitic steel plates**

Grade	Tensile test			Impact test	
	Yield Strength ( <i>N/mm<sup>2</sup></i> )	Tensile Strength ( <i>N/mm<sup>2</sup></i> )	Elongation ( $L = 5.65 \sqrt{A}$ ) (%)	Test Temp. (°C)	Average Impact Energy(J) min. <sup>(1)</sup> <i>T</i> <sup>(2)</sup>
<i>HMN40</i>	min. 400	800~970	22	-196	27

**NOTE:**

- (1) When the absorbed energy of two or more test specimens among a set of test specimens is less in value than the specified average absorbed energy or when the absorbed energy of a single test specimen is less in value than 70 % of the specified average absorbed energy, the test is considered to be failed.
- (2) T denotes that the longitudinal axis of the test specimen is arranged transverse to the final direction of rolling.

**8. Welding consumables for high manganese austenitic steel**

- (1) Where no special requirements are given in **8**, those as specified in **Pt 2, Ch 2, 607.** of the Rules apply in analogous manner.
- (2) Welding consumables are classified as specified in **Table 3.**

**Table 3 Grades and Marks of Welding Consumables**

Material for TIG welding	Flux cored wire welding	Consumables for submerged welding
<i>RYHMN</i>	<i>RWHMN</i>	<i>RUHMN</i>

- (3) Submerged arc welding consumables which have passed the tests for each welding process are to be appended with the suffixes shown in **Table 4** at the end of their marks.

**Present**

**Amendment**

**Table 4 Marks**

<u>Welding technique</u>	<u>Marks</u>
<u>Multi-run technique</u>	<u>M</u>
<u>Two-run technique</u>	<u>T</u>
<u>Multi-run and Two-run technique</u>	<u>TM</u>

**(4) Deposited metal test**

**(A) Chemical composition**

- (a) Deposited metals of welding consumables for flux cored wire welding and submerged arc welding are to have the chemical composition given in **Table 5** and **Table 6** respectively.
- (b) TIG welding consumables are to have the chemical composition of ladle analysis value complied with the requirements as given in **Table 7**.

**Table 5 Chemical Composition of Deposited Metal for Flux Cored Wire Welding**

<u>Grade</u>	<u>Chemical composition (%)</u>									
	<u>C</u>	<u>Si</u>	<u>Mn</u>	<u>P</u>	<u>S</u>	<u>Ni</u>	<u>Cr</u>	<u>Mo</u>	<u>N</u>	<u>Others</u>
<u>RW HMN</u>	<u>0.2~</u> <u>0.5</u>	<u>0.2~</u> <u>1.0</u>	<u>18.0</u> <u>~26.</u> <u>0</u>	<u>0.02</u> <u>max.</u>	<u>0.015</u> <u>max.</u>	<u>5.0</u> <u>max.</u>	<u>5.0</u> <u>max.</u>	<u>2.5</u> <u>max.</u>	<u>0.1</u> <u>max.</u>	<u>—</u>

**Table 6 Chemical Composition of Deposited Metal for Submerged Arc Welding**

<u>Grade</u>	<u>Chemical composition (%)</u>									
	<u>C</u>	<u>Si</u>	<u>Mn</u>	<u>P</u>	<u>S</u>	<u>Ni</u>	<u>Cr</u>	<u>Mo</u>	<u>N</u>	<u>Others</u>
<u>RU HMN</u>	<u>0.2~</u> <u>0.6</u>	<u>1.5</u> <u>max.</u>	<u>18.0</u> <u>~26.</u> <u>0</u>	<u>0.020</u> <u>max.</u>	<u>0.015</u> <u>max.</u>	<u>3.0</u> <u>max.</u>	<u>5.0</u> <u>max.</u>	<u>2.5</u> <u>max.</u>	<u>0.10</u> <u>max.</u>	<u>—</u>

**Present**

**Amendment**

**Table 7 Chemical Composition of Deposited Metal for TIG Electrodes**

Grade	Chemical composition (%)									
	<i>C</i>	<i>Si</i>	<i>Mn</i>	<i>P</i>	<i>S</i>	<i>Ni</i>	<i>Cr</i>	<i>Mo</i>	<i>N</i>	Others
<i>RY</i>	0.2~	0.1~	18.0	0.020	0.015	5.0	5.0	2.5	0.10	—
<i>HMN</i>	0.5	1.0	~26. 0	max.	max.	max.	max.	max.	max.	—

(B) Mechanical properties for deposited metal are to comply with the requirements in **Table 8**.

**Table 8 Mechanical properties for Deposited Metal**

Tensile test			Charpy V notch Impact test	
Yield strength (N/mm <sup>2</sup> )	Tensile strength (N/mm <sup>2</sup> )	Elongation (%)	Test temp. (°C)	Average absorbed energy (J)
400 min.	660 min.	22 min.	-196	27 min.

(5) Butt weld test

Mechanical properties for butt weld test are to comply with the requirements in **Table 9**.

**Table 9 Mechanical properties for butt weld test**

Yield strength (N/mm <sup>2</sup> )	Bend test	Charpy V notch Impact test	
		Test temp. (°C)	Average absorbed energy (J)
660 min.	The test specimens are to be capable of withstanding, without crack exceeding 3 mm long on the outer surface of the specimen or other defects.	-196	27 min.

Present	Amendment
	<p>(6) <u>Fillet weld test</u>  <u>Fillet weld test is to be in accordance with the requirements in Pt 2, Ch 2, 602. 7 of the Rules.</u></p> <p><b>9. Welder</b></p> <p>(1) <u>Welders for high manganese austenitic steel are to have a qualification by welder qualification test with high manganese austenitic steel specimen in accordance with Pt 2, Ch 2, Sec. 5 of the Rules.</u></p> <p>(2) <u>Welders who engage in welding for high manganese austenitic steel is to have passed qualification test with high manganese austenitic steel.</u></p> <p><b>10. Welding procedure qualification tests</b></p> <p>(1) <u>Welding procedure qualification tests for high manganese austenitic steel is to be in accordance with the requirements in Pt 7, Ch 5, Sec 6 of Rules and Rules/Guidances for the Classification of Ships Using Low-flashpoint Fuels.</u></p>

**Present**

**Amendment**

(2) The kinds of test and the number of test for butt welded joints is to be as shown in **Table 10**.

**Table 10 Kinds of Test for Plates with Butt Welded Joints**

Grades and material symbols of test specimens		Kinds and number of specimens for test <sup>(1)(2)</sup>						
		Visual insp.	Tensile test	Bend test	Impact test	Macro-structure insp.	Hard. test <sup>(6)</sup>	Non-destructive insp. <sup>(7)</sup>
High manganese austenitic steel	HMN40	Welding positions of whole length	3 <sup>(3)</sup>	2 <sup>(4)</sup>	5 <sup>(5)</sup>	1	1	Welding positions of whole length

**NOTES:**

- (1) Where found necessary by the Society, microscopic test, hardness test and tests other than these may be required.
- (2) Welding procedure test assembly is in accordance with **Fig 2.2.6(RL9N490)** of the Rules.
- (3) Two specimens are to be taken transversely and one specimen is to be taken longitudinally.(See **Fig 2.2.6** of the Rules)
- (4) Face bend and root bend specimens are used in accordance with **Pt 2, Ch 2, 404. 5** of the Rules.
- (5) No. of test sets and position of notch are in accordance with **Pt 7, Ch 5, Sec 6** of Rules and **Rules/Guidances for the Classification of Ships Using Low-flashpoint Fuels**.
- (6) For reference
- (7) Non-destructive inspection for detection of internal imperfections is, in principle, to be radiographic inspection. Surface inspections by penetrant examination are to be carried out.

(3) The hardness test of fillet welding is for the reference.

Present	Amendment
	<p>(4) <u>The welding procedure qualification test is carried out considering the following points.</u></p> <p>(A) <u>Special attention is to be given to the first root pass when applying flux-cored arc welding (FCAW); reduced amperage is to be considered. And weld gas composition of FCAW may be normally an 80/20 mix of argon and carbon dioxide.</u></p> <p>(B) <u>Welding heat input is to be controlled equal to maximum 30 kJ/cm or below.</u></p> <p><b>11. Welding practice</b></p> <p>(1) <u>Distance between the weld and nozzle is to be kept to a minimum to reduce the oxygen content at the vicinity of the weld pool.</u></p> <p>(2) <u>Appropriate ventilation is to be provided to reduce exposure to hazardous welding fumes.</u></p> <p>(3) <u>The edges to be welded are to be smooth, uniform and free from moisture, grease, rust and paint which may cause injurious defects in welded joints.</u></p> <p><b>12. Marking</b></p> <p>(1) <u>Steel plates which have satisfactorily complied with the required tests are to be marked with the identification mark in accordance with <b>Pt 2, Ch 1, 301. 11</b> of the Rules.</u></p> <p>(2) <u>Where the plates are controlled cooling : CC (e.g. : HMN40 CC)</u></p>